MEAM 520 More Velocity Kinematics

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Lecture 12: October 18, 2012



CHRIST CHURCH NEIGHBORHOOD HOUSE 20 NORTH AMERICAN STREET, PHILADELPHIA [OFF OF MARKET STREET AND 2ND AVENUE]



DANCE WITH CYBORGS

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DANCE WITH US: SCIENCE PER FURMS Traveling Conduct 25 at 7.50PM Traduct with Margan Bragan - edigent- space

Schurdeg October 27 at 7:50P8 Soltant with Shanah Nomia, abseptiCracty productions

Sunday October 28 at 2:30PM Performances at Christ Church Neighborhood Noces 21 North American Street, off of Narkal and 2nd Ave

525 persent, 525 Senior, 515 Studient & Dance/Feas Holders Bay Islants Here: Smyol.com/scibilance

THINK WITH US: SYMPOSIUM BERYN MILLIR COLLECE

October 27th at 2:50PM at Bryn Mawe College Hattner Halt: Darathy Versen Room, More Infecting

Linda Canvos Havland, Director of Dance of Bryn Maer College, will moderate a decoasion on digital technologies and robotics in contemporary time and moveme

n Bohaer, Chomographer & Media Arthot na Teanes, Associate Professor of Architecture, Hanaeri University ya Cuthrie, Director of The Hacktory, Philly's First Hacker Space

two event will haiture hars diseavers and beverlages, no RGNP necessary



MMERSIVE KINEMATICS

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Carbon Dance Theatre

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CARBON DANCE THEATRE creates projects that empower performers and entertain audiences by creating work that is rooted in classical ballet and infused with the collaborative process of theatre.

meredith@carbondancetheatre.com | 2920 Cambridge Street Philadelphia, PA 19130 | graphic design: tori lawrence | www.torilawrence.com

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p01-ik - meam520@seas.upenn.edu (40 messages)

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Project I : PUMA Light Painting

MEAM.Design : MEAM520-12C-P01-Sim

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MEAM.Design : MEAM520-12C-P01-Sim

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- GENERAL
- MEAM.Design MEAM 520 PUMA Light Painting: Simulation

Hell of Forme			
Hall of Fame	Now that you did your inverse kinematics		
Castactines	solution, it's time to do light painting. This	Press ENTER to ma	ke the robot move with the LED off
Contact Into	assignment is due by 5:00 p.m. on Thursday,		
COURSES	October 25. Your team must submit this		
COURSES	assignment and get it to work correctly before		
MEAM 101	you will be allowed to do the next part of the		
MEAM 201	after the deadline will be penalized, but not as		
MEAM 410/510	harshiv as for individual homework assignments.	1	
MEAM 520			
IPD 501	Your task is to write a MATLAB program that		
SAAST	create a lovely light painting (long exposure	0.8	*
	image).		
GUIDES	You should use our DUNA simulator (uf) to test	0.6	*
Materials	You should use our POMA simulator (V1) to test	(0.0	
Laser Cutting	creates an animation of the PUMA and leaves	E	
3D Printing	colored markers in the air so you can see how	N 0.4	
Machining	your creation looks. After you download the		
ProtoTRAK	simulator, run demo.m to see how it works. Read		
PUMA 260	pumasim_manual_v1.pdf to learn more about	0.2	
PHANToM	the simulator's interface. Please post on Piazza if		
BeagleBoard	you are confused about any aspect of the	0	
MAEVARM	simulator or it you find any bugs.		
Phidget	Submission	0.6	
Tap Chart	1. Start an email to	0.4	5
tup onare	meam520@seas.upenn.edu	0.2	0.5
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SolidCAM	convention	. III, where XX is your team number, plus any additional sectors and	onal lifes you may have created, also named according to this
Eagle	 In the body of the email, explain the status of 	of your submission. If you are submitting a new version	on of your IK with this assignment, state that in the email.

- 5. Send the email.
- 6. Wait for a response from the teaching team about whether your code is ready to run on the robot.

OTHER



RUNNING THE PUMA

The basic work flow when using the PUMA 260 arm is

- 1. Make sure the Emergency Stop (E-stop) button is engaged (pressed down).
- 2. Call pumaStart('Hardware', 'on', 'Delay', 10), where the number following delay is the minimum allowable time, in milliseconds, between calls to pumaServo. This may be set to any value above 0.5ms. This will display a warning that the PUMA will return to the home position. Ensure that the workspace is clear and manually move the PUMA closer to the home position if you think it may hit the table or an object.
- 3. Type 'y' or 'yes' then hit Enter to continue.
- 4. Release the E-stop by pulling up on the button, at which time the PUMA will return to the home position.
- 5. In a separate MATLAB process, call startFrameBuffer to begin capturing video from the webcam.
- 6. Make a light painting, using pumaServo to command the robot to move. Remember to call pumaLEDOn to enable the LED and use pumaLEDSet to select the color.
- 7. Call stopFrameBuffer to finish capturing video.
- 8. Return the PUMA to the home position, if possible.
- 9. Call pumaStop to disable the controller.
- 10. Engage the E-stop by pressing the button down.
- 11. Use makeVideoAndImage to create long-exposure picture and video. Optionally, you may wish to save the image files to a different location using saveImagesToFolder before starting a new video.

There are several other things to keep in mind:

- Do <u>NOT</u> use the clear all command once the PUMA has been initialized before calling pumaStop, otherwise MATLAB will crash.
- Test the video capture before running your whole light painting.

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Confirmed Midterm Date Thursday, November 8, in class

 \sim email KJK if you have a severe conflict \sim

Velocity Kinematics



Slides created by Jonathan Fiene How do the velocities of the joints affect the linear and angular velocity of the end-effector?

These quantities are related by the **Jacobian**, a matrix that generalizes the notion of an ordinary derivative of a scalar function.

Jacobians are useful for planning and executing smooth trajectories, determining singular configurations, executing coordinated anthropomorphic motion, deriving dynamic equations of motion, and transforming forces and torques from the end-effector to the manipulator joints. explore how **changes** in joint values affect the end-effector movement

could have **N joints**, but only **six** end-effector velocity terms (xyzpts)

The **Jacobian** matrix lets us calculate how joint velocities translate into end-effector velocities (depends on configuration)

look at it in two parts - position and orientation

$$v_n^0 = J_v \dot{q} \qquad \qquad \omega_n^0 = J_\omega \dot{q}$$

How do we calculate the position Jacobian?



$$\mathbf{J}_{p} = \begin{bmatrix} \frac{\delta x}{\delta q_{1}} & \frac{\delta x}{\delta q_{2}} & \cdots & \frac{\delta x}{\delta q_{n}} \\ \frac{\delta y}{\delta q_{1}} & \frac{\delta y}{\delta q_{2}} & \cdots & \frac{\delta y}{\delta q_{n}} \\ \frac{\delta z}{\delta q_{1}} & \frac{\delta z}{\delta q_{2}} & \cdots & \frac{\delta z}{\delta q_{n}} \end{bmatrix}$$

Prismatic

$$J_{v_i} = z_{i-1}$$

Revolute $J_{v_i} = z_{i-1} \times (o_n - o_{i-1})$

$$v_n^0 = J_v \dot{q}$$

What joint velocities should I choose to cause a desired end-effector velocity? (inverse velocity kinematics)

$$\dot{q} = J_v^{-1} v_n^0$$

This works only when the Jacobian is square and invertible (non-singular).

SHV 4.11 explains what to do when the Jacobian is not square: rank test (v is in range of J) use J⁺ (right pseudoinverse of J) when the robot has extra joints, there are many solutions Singularities are points in the configuration space where infinitesimal motion in a certain direction is not possible and the manipulator loses one or more degrees of freedom

Mathematically, singularities exist at any point in the workspace where the Jacobian matrix loses rank.

a matrix is singular if and only if its determinant is zero: $det(\mathbf{J}) = 0$



Is that the only time?

No... $det(\mathbf{J}) = 0$ when $\theta_2 = ..., -2\pi, -\pi, 0, \pi, 2\pi, ...$

Any other times? $det(\mathbf{J}) = 0$ when $a_1 = 0$ or $a_2 = 0$

For
$$\theta_2=0$$

The Jacobian collapses to have linearly dependent rows

$$\mathbf{J}_{\theta_2=0} = \begin{bmatrix} -a_1 s_1 - a_2 s_1 & -a_2 s_1 \\ a_1 c_1 + a_2 c_1 & a_2 c_1 \end{bmatrix}$$

This means that actuating either joint causes motion in the same direction



Questions ?

explore how **changes** in joint values affect the end-effector movement

could have **N joints**, but only **six** end-effector velocity terms (xyzpts)

The **Jacobian** matrix lets us calculate how joint velocities translate into end-effector velocities (depends on configuration)

look at it in two parts - position and orientation

$$v_n^0 = J_v \dot{q} \qquad \qquad \omega_n^0 = J_\omega \dot{q}$$

How do we calculate the orientation Jacobian?



 $\omega_{i,j}^k$

this is the angular velocity of frame **j** with respect to frame **i**, expressed in frame **k**

SHV 4.1 gives a good explanation of angular velocity for fixed-axis rotation. SHV 4.2-4.5 go into greater detail.

The Angular Velocity of Connected Rigid Bodies



$$\omega_{0,n}^{0} = \sum_{i=1}^{n} \mathbf{R}_{i-1}^{0} \omega_{i-1,i}^{i-1}$$
$$\omega_{0,n}^{0} = \sum_{i=1}^{n} (\mathbf{R}_{i-1}^{0} \hat{\mathbf{z}}) \dot{\theta}_{i}$$

note: this holds for revolute joints only (by definition, a prismatic joint cannot create angular velocity)

i=1

$$\omega_{0,n}^0 = \sum_{i=1}^n \rho_i (\mathbf{R}_{i-1}^0 \hat{z}) \, \dot{\theta}_i \qquad \rho_i = \frac{0 \text{ for prismatic}}{1 \text{ for revolute}}$$

$$\omega_{0,n}^{0} = \begin{bmatrix} \rho_{1} \hat{\mathbf{z}} & \rho_{2} \mathbf{R}_{1}^{0} \hat{\mathbf{z}} & \rho_{2} \mathbf{R}_{2}^{0} \hat{\mathbf{z}} & \dots & \rho_{n} \mathbf{R}_{n-1}^{0} \hat{\mathbf{z}} \end{bmatrix} \begin{bmatrix} \dot{\theta}_{1} \\ \dot{\theta}_{2} \\ \vdots \\ \dot{\theta}_{n} \end{bmatrix}$$

 $\omega = \mathbf{J}_{\omega}(q) \, \dot{\mathbf{q}}$



The Jacobian is easily constructed from the manipulator's forward kinematics.

What do you need from the forward kinematics?

4.6.3 Combining the Linear and Angular Velocity Jacobians As we have seen in the preceding section, the upper half of the Jacobian J_v is given as

$$J_{\mathcal{V}} = [J_{\mathcal{V}_1} \cdots J_{\mathcal{V}_n}] \tag{4.56}$$

in which the i^{th} column J_{v_i} is

$$J_{v_i} = \begin{cases} z_{i-1} \times (o_n - o_{i-1}) & \text{for revolute joint} \\ z_{i-1} & \text{for prismatic joint } i \end{cases}$$
(4.57)

The lower half of the Jacobian is given as

$$J_{\omega} = [J_{\omega_1} \cdots J_{\omega_n}] \tag{4.58}$$

in which the i^{th} column J_{ω_i} is

$$J_{\omega_i} = \begin{cases} z_{i-1} & \text{for revolute joint } i \\ 0 & \text{for prismatic joint } i \end{cases}$$
(4.59)

Singularities are points in the configuration space where infinitesimal motion in a certain direction is not possible and the manipulator loses one or more degrees of freedom

Mathematically, singularities exist at any point in the workspace where the Jacobian matrix loses rank.

a matrix is singular if and only if its determinant is zero: $det(\mathbf{J}) = 0$



$$\left[\begin{array}{c} v_n^0\\ \omega_n^0 \end{array}\right] = \left[\begin{array}{c} J_v\\ J_\omega \end{array}\right]\dot{q}$$

For a 6-DOF manipulator with a spherical wrist, we can decouple the determination of singular configurations into two simpler problems.

$$J = [J_{\rm arm} \mid J_{\rm wrist}]$$

(the book calls this
$$J = [J_P \mid J_O]$$
)
$$J = [J_{\text{arm}} \mid J_{\text{wrist}}] = \left[\frac{J_{11}}{J_{21}} \mid \frac{J_{12}}{J_{22}}\right]$$

$$J_{\text{wrist}} = \begin{bmatrix} z_3 \times (o_6 - o_3) & z_4 \times (o_6 - o_4) & z_5 \times (o_6 - o_5) \\ z_3 & z_4 & z_5 \end{bmatrix}$$

if we choose $o_4 = o_5 = o_6$

$$J_{\text{wrist}} = \begin{bmatrix} 0 & 0 & 0 \\ z_3 & z_4 & z_5 \end{bmatrix}$$

 $J = \left[\frac{J_{11}}{J_{21}} | \frac{0}{J_{22}}\right] \qquad \det(J) = \det(J_{11}) \det(J_{22})$

$$\det(J) = \det(J_{11}) \det(J_{22})$$

$$J_{22} = \left[\begin{array}{ccc} z_3 & z_4 & z_5 \end{array} \right]$$

Singular when any two wrist axes align



 z_3 can become $|| z_5$

 $\theta_5 = 0, \pi$ are singular configurations

For a specific configuration, the Jacobian scales the input (joint velocities) to the output (body velocity)

$$\xi = J(q)\dot{q}$$

If you put in a joint velocity vector with unit norm, you can calculate in which direction and how fast the robot will translate and rotate.

If the Jacobian is full rank, you can calculate the manipulability ellipsoid.

choose $\dot{q} = J^+ \xi$ $||\dot{q}||^2 = \xi^T (JJ^T)^{-1} \xi$

If not redundant, manipulability $\mu = |\det(J)|$

What does the manipulability ellipsoid look like for the planar RR robot?





$$\mu = |\det(J)| = a_1 a_2 |\sin(\theta_2)|$$

Can be used to tell you where to perform certain tasks.

Also useful for deciding how to design a manipulator. Soon I will release Homework 4, an individual assignment on Jacobians

Not sure when it will be due...

Homework 2 and 3 graded