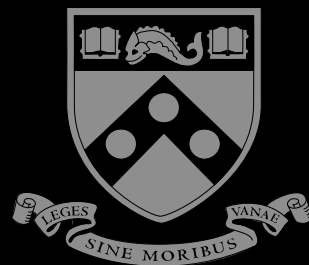


MEAM 520

Velocity Kinematics

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MEAM Department, SEAS, University of Pennsylvania



MEAM.Design : MEAM520-12C-P01-IK

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Materials
Laser Cutting
3D Printing
Machining
ProtoTRAK
PUMA 260
PHANTOM
BeagleBoard
MAEVARM
Phidget
Tap Chart

SOFTWARE

SolidWorks

MEAM.Design - MEAM 520 - PUMA Light Painting: IK

Now that you have your team, it's time to get to work on project 1. This assignment is due by **5:00 p.m. on Tuesday, October 16**. Your team must submit this assignment and get it to work correctly before you will be allowed to do the next part of the project. Submissions after the deadline will be penalized, but not as harshly as for individual homework assignments.

The final goal of this project is to create a beautiful light painting by taking a long-exposure video and photo of the PUMA moving an LED around in the air. As an intermediate step toward that goal, you and your teammates must solve the inverse kinematics of the robot, so that you can later safely move its end-effector wherever is needed for your artwork.

LED Location

The center of the LED is located at approximately $[0 \text{ in. } 0.125 \text{ in. } 1.25 \text{ in.}]^T$ in frame 6. The position and orientation of frames 0 and 6 are specified in the image at right, as are the positive directions for all the joints. These conventions match what was specified in Homework 3.

Joint Angle Limits

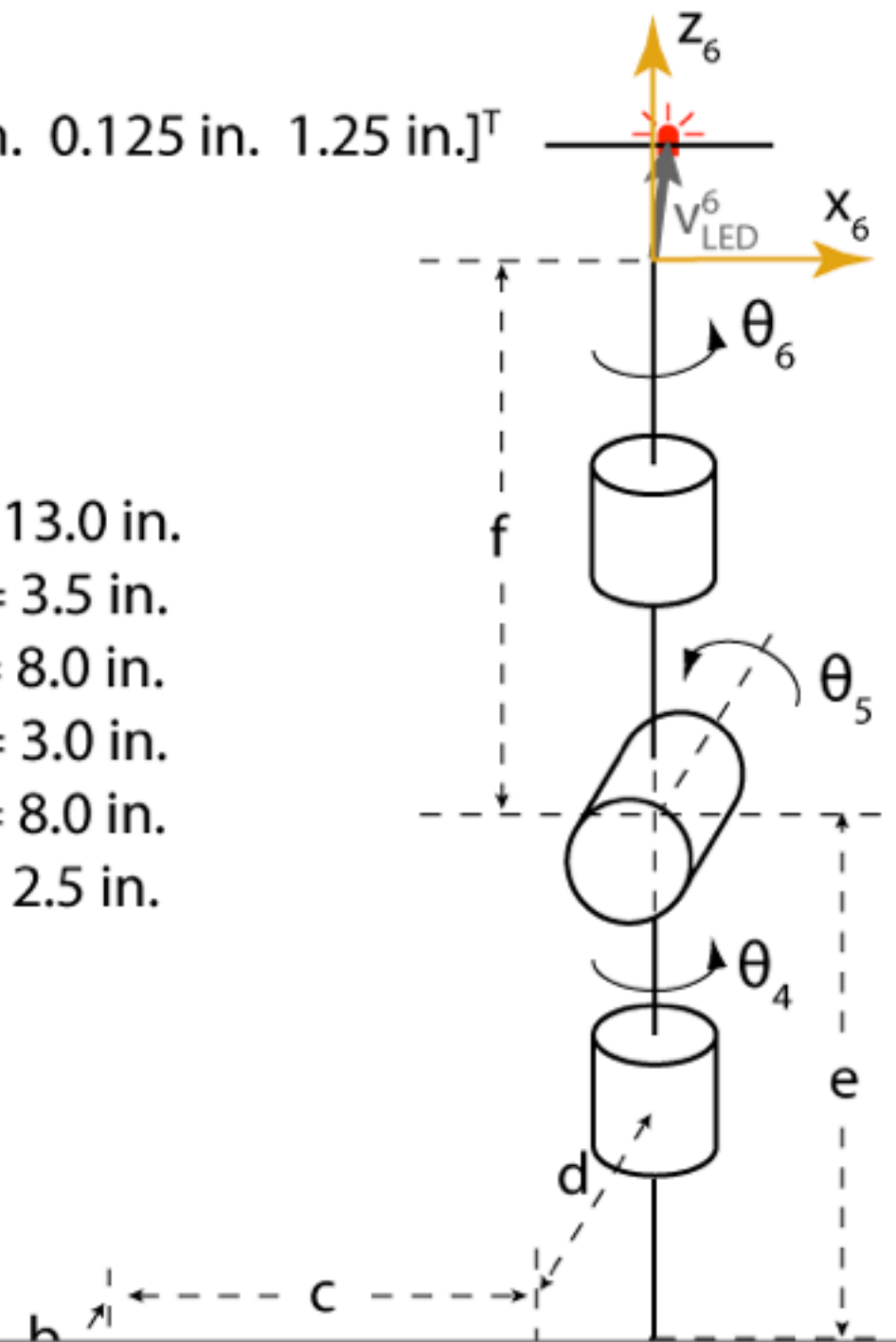
θ_1 (waist) range = 290 deg , lowerlimit = -180 deg , upperlimit = 110 deg
 θ_2 (shoulder) range = 315 deg , lowerlimit = -75 deg , upperlimit = 240 deg
 θ_3 (elbow) range = 295 deg , lowerlimit = -235 deg , upperlimit = 60 deg
 θ_4 (wrist) range = 620 deg , lowerlimit = -580 deg , upperlimit = 40 deg
 θ_5 (bend) range = 230 deg , lowerlimit = -120 deg , upperlimit = 110 deg
 θ_6 (flange) range = 510 deg , lowerlimit = -215 deg , upperlimit = 295 deg

PUMA 260 Simulator

At some point soon, we will publish a full forward kinematics simulator for the PUMA 260 robot. It will have the same software interface as our real PUMA robot. You may find it useful to use the simulator to verify your forward kinematics and inverse kinematics solutions. More details will be

$$\mathbf{v}_{LED}^6 = [0 \text{ in. } 0.125 \text{ in. } 1.25 \text{ in.}]^T$$

$a = 13.0 \text{ in.}$
 $b = 3.5 \text{ in.}$
 $c = 8.0 \text{ in.}$
 $d = 3.0 \text{ in.}$
 $e = 8.0 \text{ in.}$
 $f = 2.5 \text{ in.}$



Editor - /Users/kuchenbe/Documents/teaching/meam 520/projects/01 light painting/01 ik/puma_fk_team00.m

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1.0 1.1

```
1 function T06 = puma_fk_team00(th1, th2, th3, th4, th5, th6)
2 %% PUMA_FK_TEAM00 Calculates the forward kinematics for the PUMA 260.
3 %
4 % This Matlab file provides the starter code for the PUMA 260 forward
5 % kinematics function of project 1 in MEAM 520 at the University of
6 % Pennsylvania. The original was written by Professor Katherine J.
7 % Kuchenbecker in October of 2012. Students will work in teams modify this
8 % code to create their own script. Post questions on the class's Piazza
9 % forum.
10 %
11 % The six inputs (th1 ... th6) are the PUMA's current joint angles in
12 % radians, specified according to the order and sign conventions described
13 % in the documentation.
14 %
15 % The one output is the homogeneous transformation representing the pose of
16 % frame 6 in frame 0. The position part of this transformation is in
17 % inches.
18 %
19 % Please change the name of this file and the function declaration on the
20 % first line above to include your team number rather than 00. Also list
21 % your team number and the full names of your three team members below.
22 %
23 % Team Number:
24 % Team Members:
25
26
27 %% ROBOT PARAMETERS
28 % This problem is about the PUMA 260 robot, a 6-DOF manipulator.
29
30 % Define the robot's measurements. These correspond to the diagram in the
31 % homework and are constant.
32 a = 13.0; % inches
33 b = 3.5; % inches
34 c = 8.0; % inches
35 d = 3.0; % inches
```

puma_fk_team00.m puma_ik_team00.m test_puma_ik_team00.m

puma_fk_team00 Ln 28 Col 18

Editor - /Users/kuchenbe/Documents/teaching/meam 520/projects/01 light painting/01 ik/puma_ik_team00.m

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1.0 1.1

```
1 function [th1 th2 th3 th4 th5 th6] = puma_ik_team00(x, y, z, phi, theta, psi)
2 %% PUMA_IK_TEAM00 Calculates the full inverse kinematics for the PUMA 260.
3 %
4 % This Matlab file provides the starter code for the PUMA 260 inverse
5 % kinematics function of project 1 in MEAM 520 at the University of
6 % Pennsylvania. The original was written by Professor Katherine J.
7 % Kuchenbecker in October of 2012. Students will work in teams modify this
8 % code to create their own script. Post questions on the class's Piazza
9 % forum.
10 %
11 % The first three input arguments (x, y, z) are the desired coordinates of
12 % the PUMA's end-effector tip in inches, specified in the base frame. The
13 % origin of the base frame is where the first joint axis (waist) intersects
14 % the table. The z0 axis points up, and the x0 axis points out away from
15 % the robot, perpendicular to the front edge of the table. These arguments
16 % are mandatory.
17 %
18 % The fourth through sixth input arguments (phi, theta, psi) represent the
19 % desired orientation of the PUMA's end-effector in the base frame using
20 % ZYZ Euler angles in radians. These arguments are mandatory.
21 %
22 % The seventh through twelfth input arguments (th1now ... th6now) are the
23 % current joint angles of the PUMA. These arguments are optional, but you
24 % must supply all of them if you supply any of them. Passing in the
25 % robot's current joint angles enables this function to find an IK solution
26 % close to the robot's current configuration, to avoid large jumps in the
27 % robot's movement. If these values are not passed in, the function may
28 % select from the possible solutions in any manner.
29 %
30 % The six outputs (th1 ... th6) are the joint angles needed to place the
31 % PUMA's end-effector at the desired position and in the desired
32 % orientation. These joint angles are specified in radians according to the
33 % order and sign conventions described in the documentation. If this
34 % function cannot find a solution to the inverse kinematics problem, it
```

puma_fk_team00.m puma_ik_team00.m test_puma_ik_team00.m

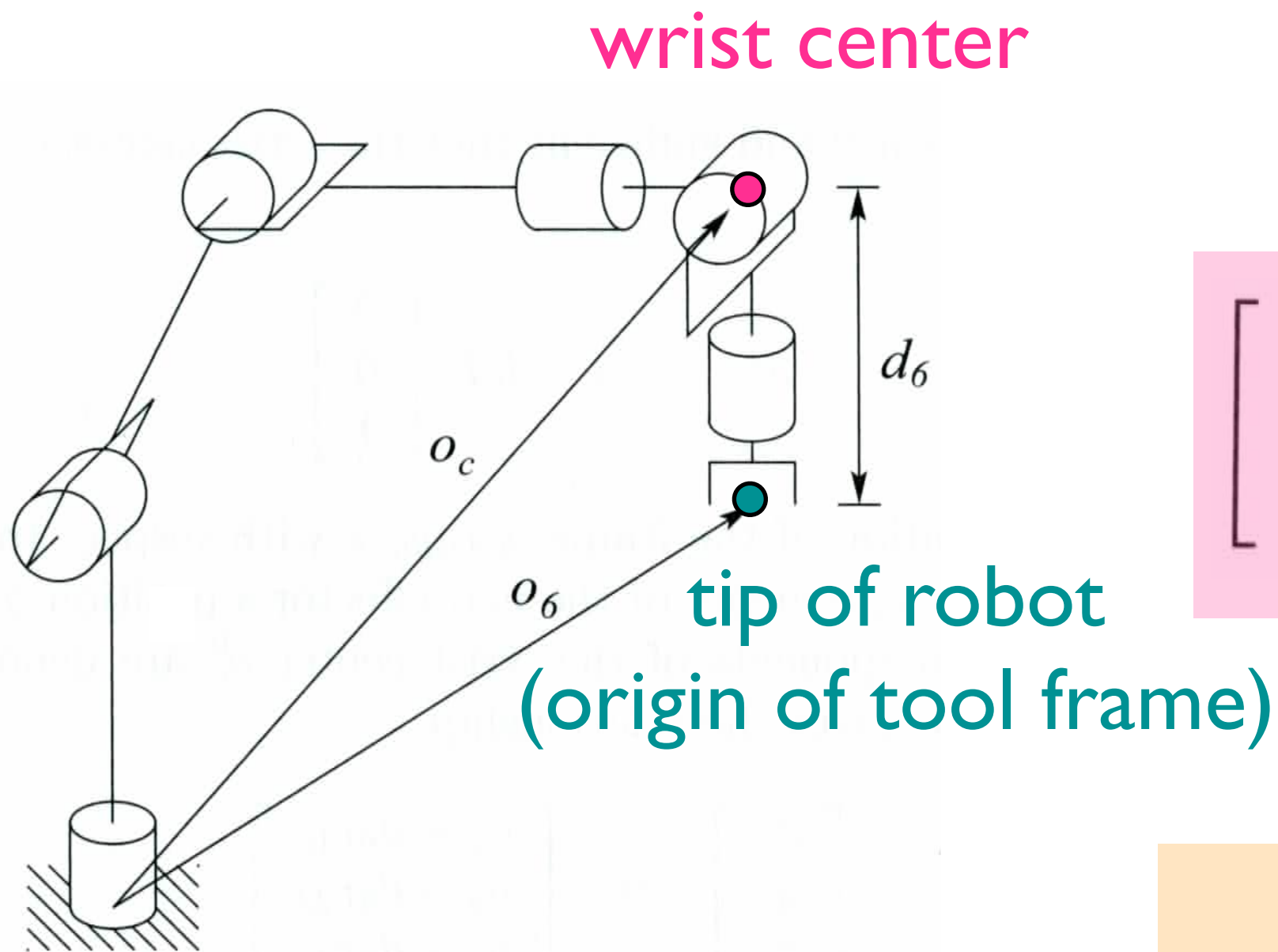
puma_ik_team00 Ln 20 Col 31

File Edit Text Go Cell Tools Debug Desktop Window Help

```

1 %% TEST_PUMA_IK_TEAM00 Tests the full inverse kinematics for the PUMA 260.
2 %
3 % This Matlab file provides the starter code for the PUMA 260 inverse
4 % kinematics testing script of project 1 in MEAM 520 at the University of
5 % Pennsylvania. The original was written by Professor Katherine J.
6 % Kuchenbecker in October of 2012. Students will work in teams modify this
7 % code to create their own script. Post questions on the class's Piazza
8 % forum.
9 %
10 % This script runs thorough tests on the inverse kinematics function the
11 % designated team has written for the PUMA 260. At a minimum, it
12 % calculates the following two scores:
13 %
14 % score_without_thnow
15 % The score for the inverse kinematics solution when called without the
16 % current configuration of the robot (th1now ... th6now). The ik function
17 % is free to pick any valid solution. It should return NaN for all six
18 % joint angles if the requested configuration is not reachable or is
19 % outside the robot's joint limits. The score should range from 0 (worst
20 % performance) to 100 (perfect performance).
21 %
22 % score_with_thnow
23 % The score for the inverse kinematics solution when called with the
24 % current configuration of the robot (th1now ... th6now). The ik function
25 % should pick the valid solution closest to the current joint angles. The
26 % function should return NaN for all six joint angles if the requested
27 % configuration is not reachable or is outside the robot's joint limits.
28 % The score should range from 0 (worst performance) to 100 (perfect
29 % performance).
30 %
31 % Please change the name of this file to include your team number rather
32 % than 00. Also list your team number and the full names of your three
33 % team members below.
34 %

```



$$o = o_c^0 + d_6 R \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

$$\begin{bmatrix} x_c \\ y_c \\ z_c \end{bmatrix} = \begin{bmatrix} o_x - d_6 r_{13} \\ o_y - d_6 r_{23} \\ o_z - d_6 r_{33} \end{bmatrix}$$

position

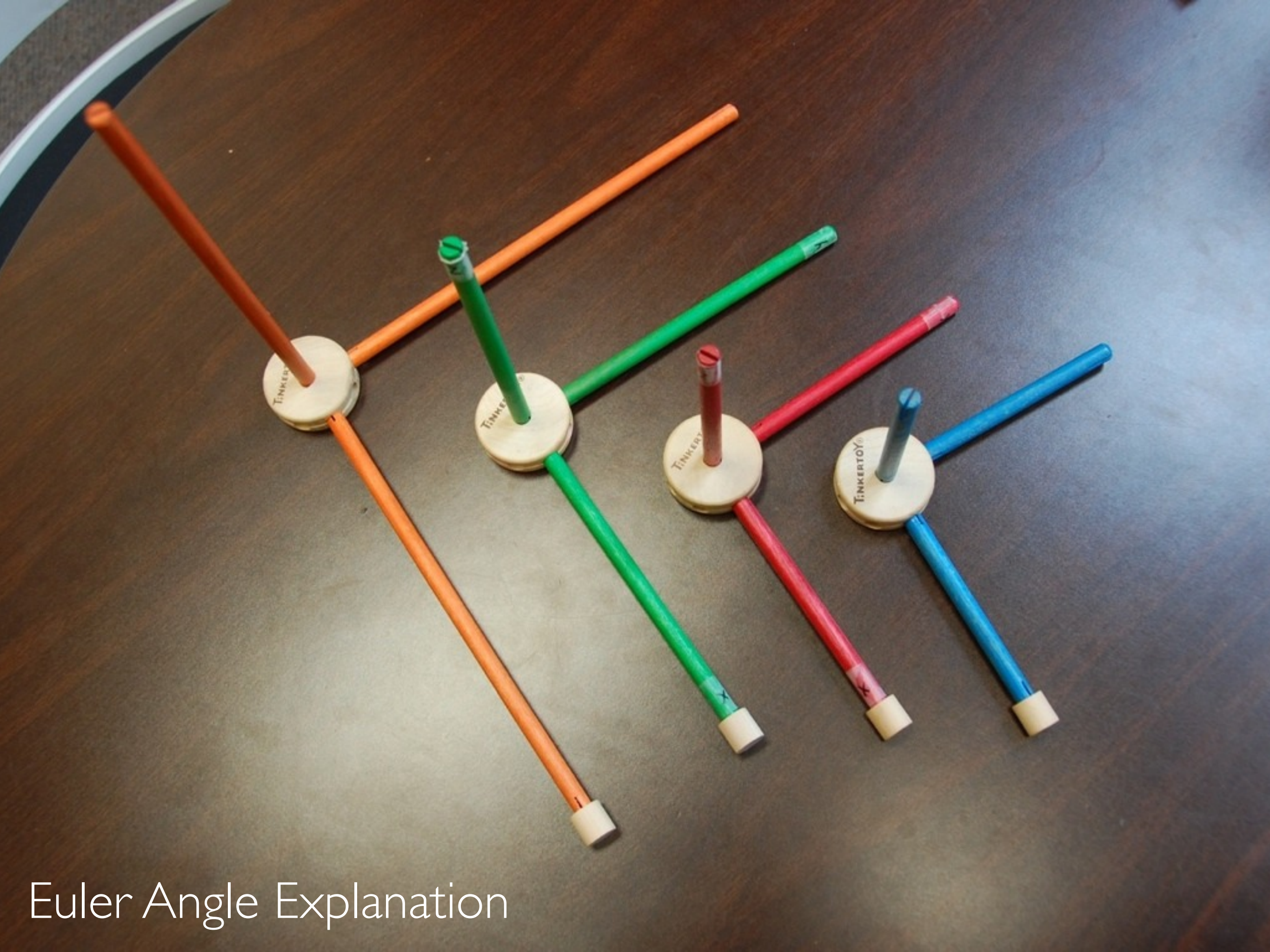
$$R = R_3^0 R_6^3$$

$$R_6^3 = (R_3^0)^{-1} R = (R_3^0)^T R$$

orientation



Quick Example with a MATLAB Rubik's Cube



Euler Angle Explanation

$$\begin{aligned}
T_6^3 &= A_4 A_5 A_6 \\
&= \begin{bmatrix} R_6^3 & o_6^3 \\ 0 & 1 \end{bmatrix} \\
&= \begin{bmatrix} c_4 c_5 c_6 - s_4 s_6 & -c_4 c_5 s_6 - s_4 c_6 & c_4 s_5 & c_4 s_5 d_6 \\ s_4 c_5 c_6 + c_4 s_6 & -s_4 c_5 s_6 + c_4 c_6 & s_4 s_5 & s_4 s_5 d_6 \\ -s_5 c_6 & s_5 s_6 & c_5 & c_5 d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}
\end{aligned}$$

$$\theta_4 = \phi \quad \theta_5 = \theta \quad \theta_6 = \psi$$

$$= \begin{bmatrix} c_\phi c_\theta c_\psi - s_\phi s_\psi & -c_\phi c_\theta s_\psi - s_\phi c_\psi & c_\phi s_\theta \\ s_\phi c_\theta c_\psi + c_\phi s_\psi & -s_\phi c_\theta s_\psi + c_\phi c_\psi & s_\phi s_\theta \\ -s_\theta c_\psi & s_\theta s_\psi & c_\theta \end{bmatrix}$$

The book explains how to calculate the three angles given **R**: see SHV pages 55-56

Turn in your best effort by 5:00 p.m. today.

Using your IK for light painting may expose issues; you will be able to submit a new IK solution and test function with your final code for project I.

Questions ?



Project I : PUMA Light Painting



PUMA Light Painting code due
by 5:00 p.m. on Thursday, October 25.
Submissions after that are late.

Same teams as IK.

Develop in simulation, get approval,
meet with a member of the teaching
team to learn to run the real robot
and make your light painting.

Code review will be ongoing; submit
as soon as you are happy.

PUMA simulator to be released soon.



If your IK solution is good, this part of the project should be fun and easy.

If your IK solution isn't working well yet, you will need to get it to work to be able to use the robot.

We will make a gallery of MEAM 520 PUMA light paintings.

Creative ideas for light painting?

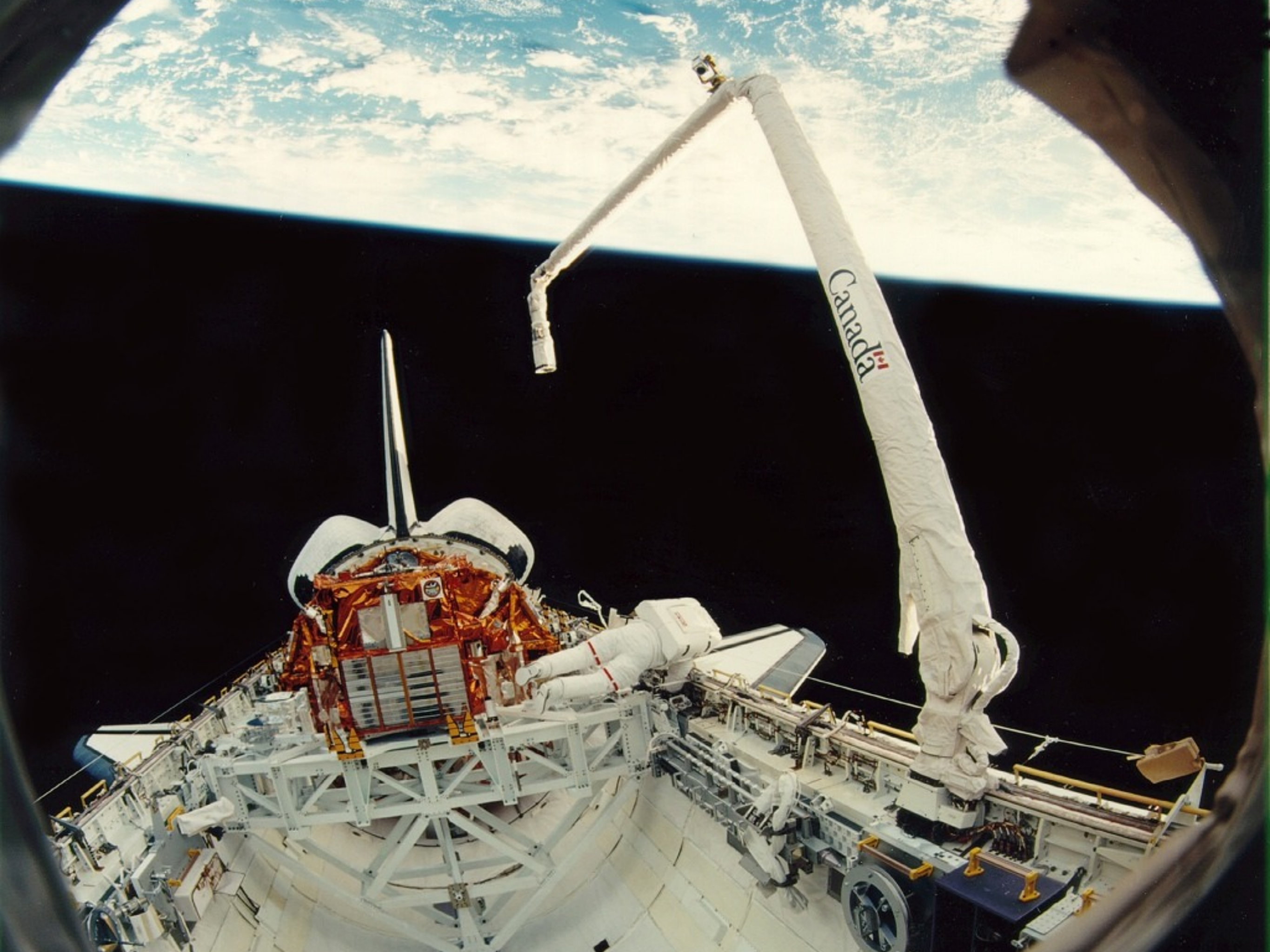
Proposed Midterm Date
Thursday, November 8, in class



Velocity Kinematics



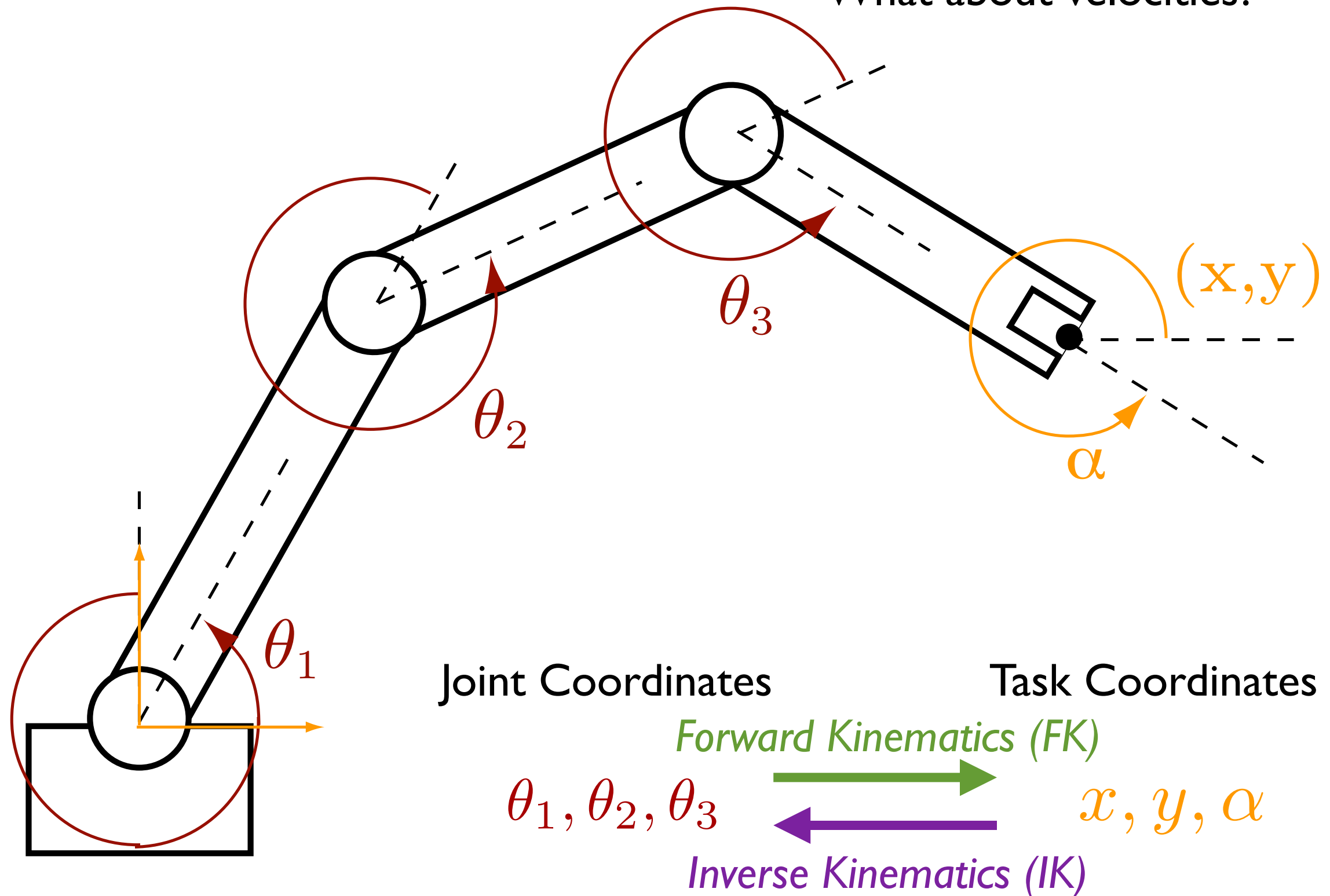
Slides created by
Jonathan Fiene





Joint and Task Coordinates

So much about position and orientation.
What about velocities?

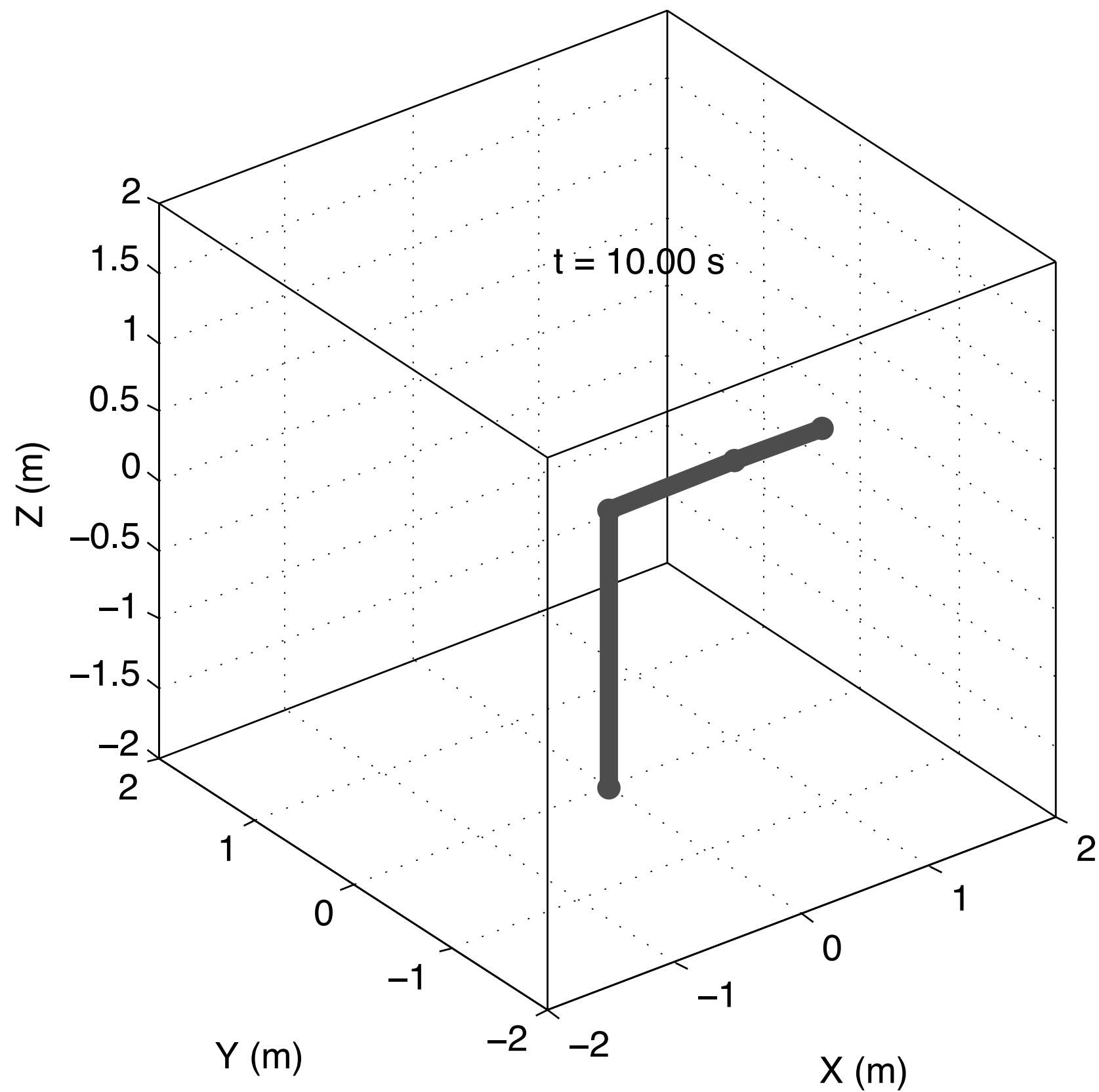


How do the velocities of the joints affect the linear and angular velocity of the end-effector?

These quantities are related by the **Jacobian**, a matrix that generalizes the notion of an ordinary derivative of a scalar function.

Jacobians are useful for planning and executing smooth trajectories, determining singular configurations, executing coordinated anthropomorphic motion, deriving dynamic equations of motion, and transforming forces and torques from the end-effector to the manipulator joints.

SCARA Robot Moving Just a Little Bit



explore how **changes** in joint values affect the end-effector movement (velocities)

could have **N joints**, but only **six** end-effector velocity terms (xyzpts)

would love to have a matrix that goes from joint velocities to end-effector velocities!

look at it in two parts - position and orientation

$$v_n^0 = J_v \dot{q}$$

$$\omega_n^0 = J_\omega \dot{q}$$

for

$$x(t) = f(q_1(t), q_2(t), \dots, q_n(t))$$

the time derivative can be found using

$$\frac{dx}{dt} = \sum_{i=1}^n \frac{\delta x}{\delta q_i} \frac{dq_i}{dt}$$

For an n-dimensional joint space and a cartesian workspace, the position Jacobian is a 3xn matrix composed of the partial derivatives of the end-effector position with respect to each joint variable.

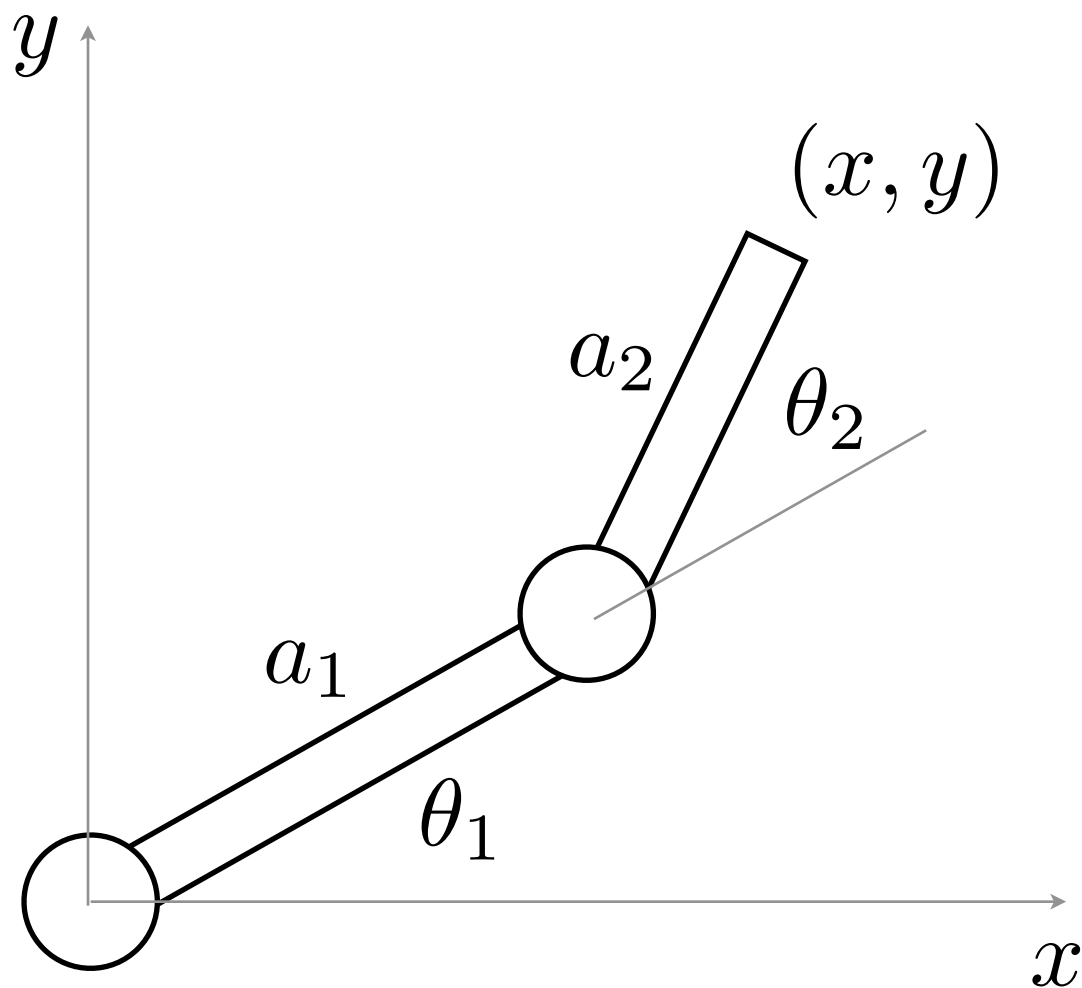
$$\mathbf{J}_p = \begin{bmatrix} \frac{\delta x}{\delta q_1} & \frac{\delta x}{\delta q_2} & \cdots & \frac{\delta x}{\delta q_n} \\ \frac{\delta y}{\delta q_1} & \frac{\delta y}{\delta q_2} & \cdots & \frac{\delta y}{\delta q_n} \\ \frac{\delta z}{\delta q_1} & \frac{\delta z}{\delta q_2} & \cdots & \frac{\delta z}{\delta q_n} \end{bmatrix}$$

$$\dot{\mathbf{p}} = \mathbf{J}_p(q) \dot{\mathbf{q}}$$

Diagram illustrating the relationship between endpoint velocity, Jacobian matrix, and joint velocity:

- $\dot{\mathbf{p}}$ is labeled as endpoint velocity.
- $\mathbf{J}_p(q)$ is labeled as Jacobian matrix.
- $\dot{\mathbf{q}}$ is labeled as joint velocity.

The Position Jacobian : Planar RR



$$\mathbf{J}_p = \begin{bmatrix} \frac{\delta x}{\delta q_1} & \frac{\delta x}{\delta q_2} & \cdots & \frac{\delta x}{\delta q_n} \\ \frac{\delta y}{\delta q_1} & \frac{\delta y}{\delta q_2} & \cdots & \frac{\delta y}{\delta q_n} \\ \frac{\delta z}{\delta q_1} & \frac{\delta z}{\delta q_2} & \cdots & \frac{\delta z}{\delta q_n} \end{bmatrix}$$

which relates instantaneous joint velocities to endpoint velocities

$$\begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} -a_1 s_1 - a_2 s_{12} & -a_2 s_{12} \\ a_1 c_1 + a_2 c_{12} & a_2 c_{12} \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix}$$

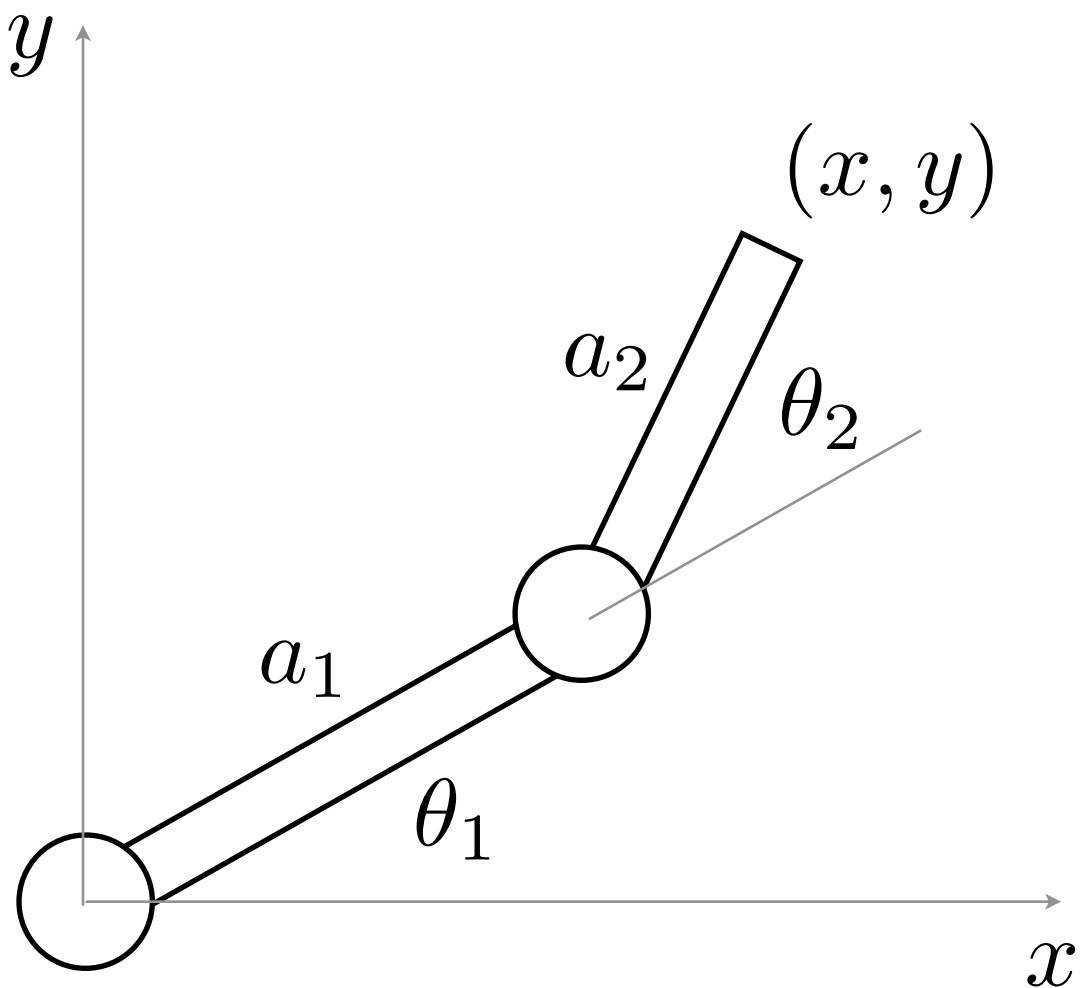
From the forward kinematics, we can extract the position vector from the last column of the transform matrix:

$$\mathbf{d}_2^0 = \begin{bmatrix} a_2 c_{12} + a_1 c_1 \\ a_2 s_{12} + a_1 s_1 \\ 0 \end{bmatrix}$$

Taking the partial derivative with respect to each joint variable produces the Jacobian:

$$\mathbf{J} = \begin{bmatrix} -a_1 s_1 - a_2 s_{12} & -a_2 s_{12} \\ a_1 c_1 + a_2 c_{12} & a_2 c_{12} \\ 0 & 0 \end{bmatrix}$$

The Position Jacobian : Planar RR



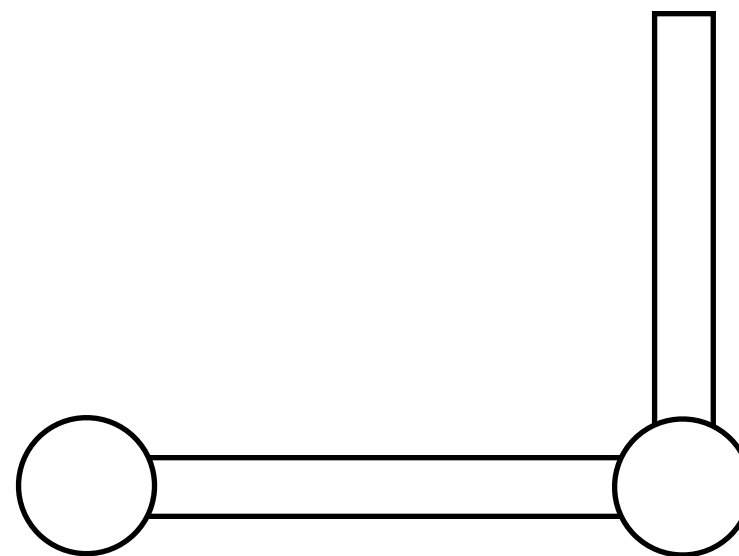
$$\mathbf{J} = \begin{bmatrix} -a_1 s_1 - a_2 s_{12} & -a_2 s_{12} \\ a_1 c_1 + a_2 c_{12} & a_2 c_{12} \\ 0 & 0 \end{bmatrix}$$

$$\theta_1 = 0, \theta_2 = \pi/2$$

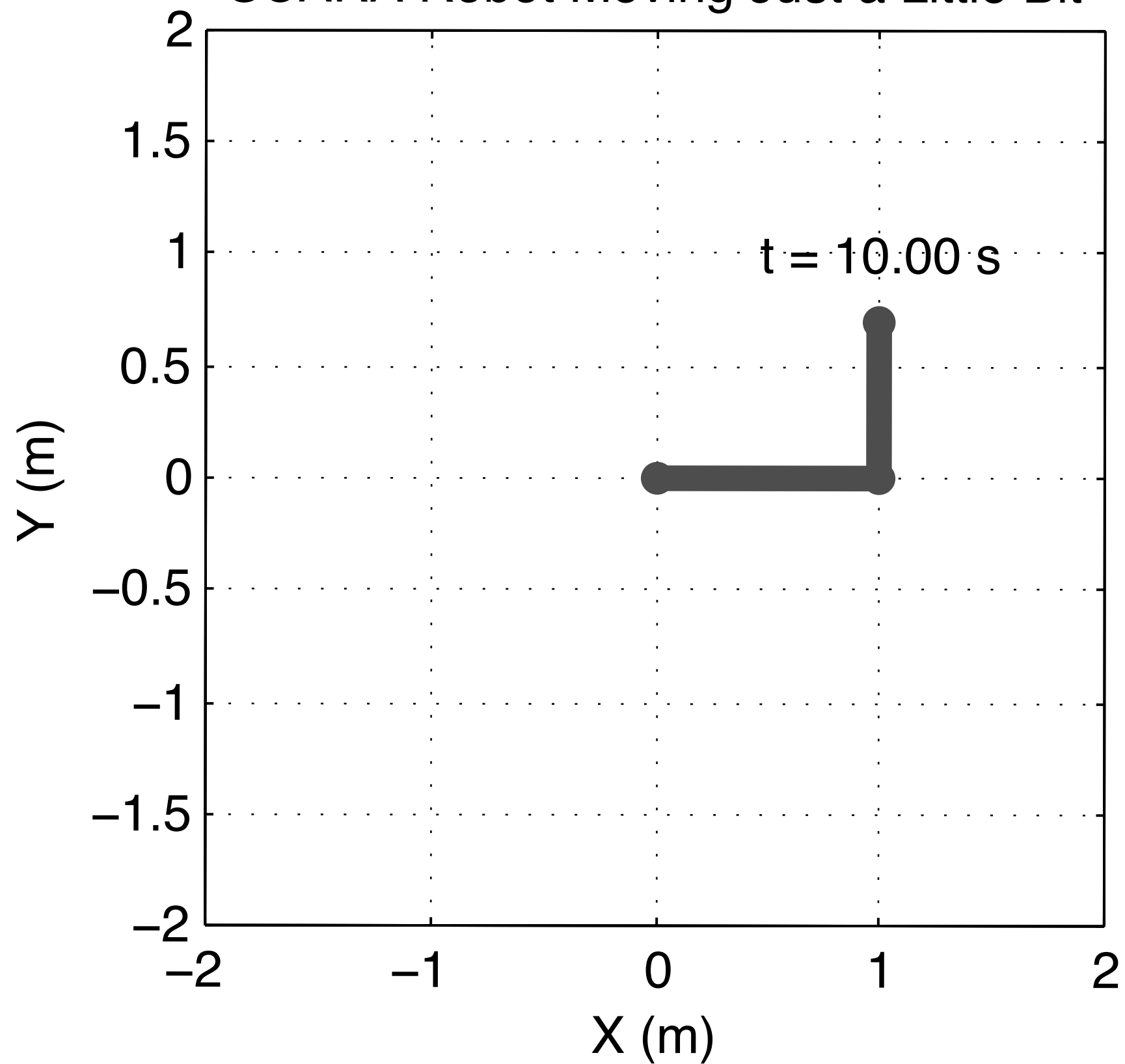
$$\dot{x} = -a_2 \dot{\theta}_1 - a_2 \dot{\theta}_2$$

$$\dot{y} = a_1 \dot{\theta}_1$$

$$\dot{z} = 0$$



SCARA Robot Moving Just a Little Bit



Position Jacobian for SCARA?

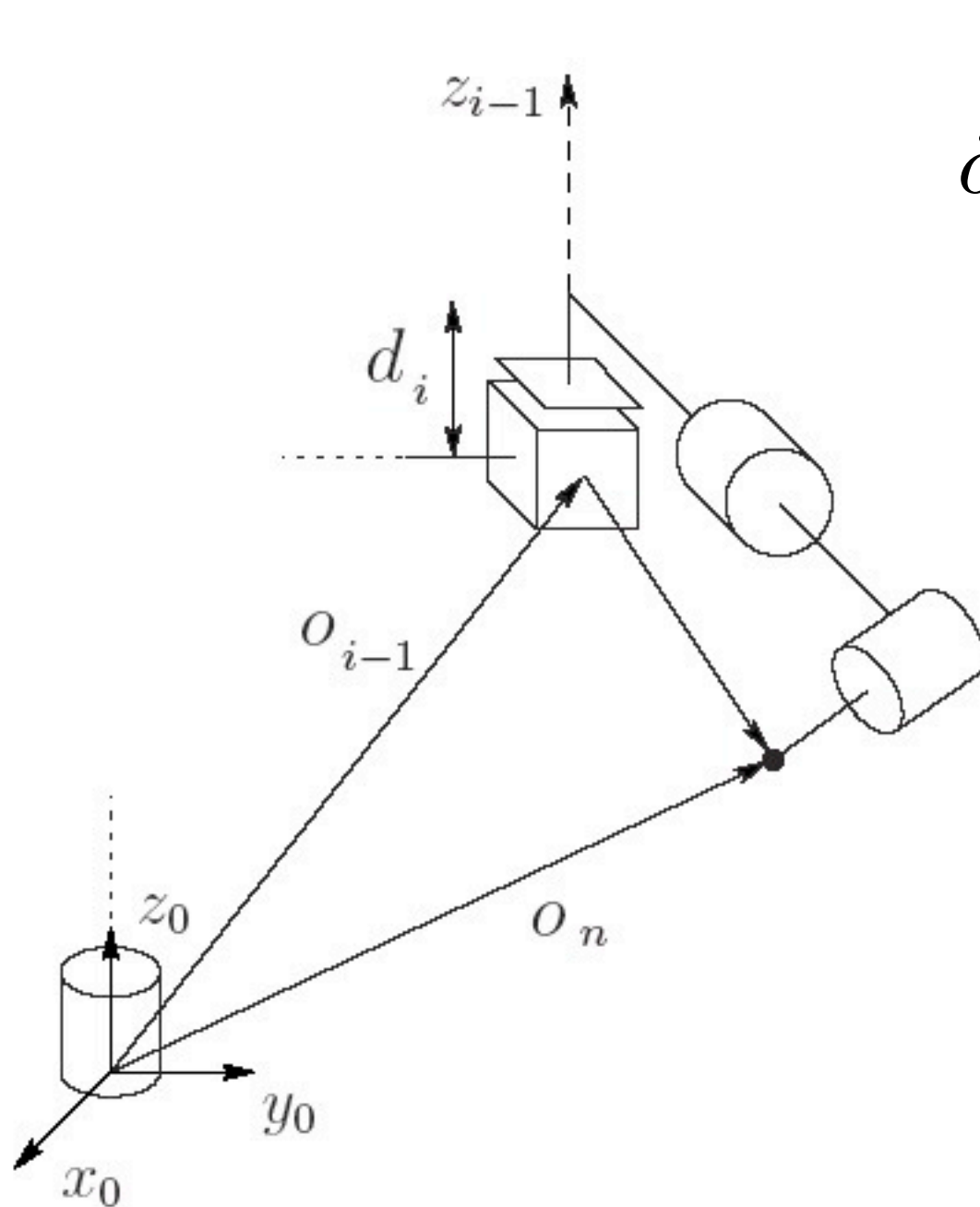
Work with a partner. Where do you start?

$$\begin{bmatrix} x \\ y \\ z \end{bmatrix} = \begin{bmatrix} a_1 c_1 + a_2 c_{12} \\ a_1 s_1 + a_2 s_{12} \\ -d_3 \end{bmatrix}$$

$$\mathbf{J}_p = \begin{bmatrix} \frac{\delta x}{\delta q_1} & \frac{\delta x}{\delta q_2} & \cdots & \frac{\delta x}{\delta q_n} \\ \frac{\delta y}{\delta q_1} & \frac{\delta y}{\delta q_2} & \cdots & \frac{\delta y}{\delta q_n} \\ \frac{\delta z}{\delta q_1} & \frac{\delta z}{\delta q_2} & \cdots & \frac{\delta z}{\delta q_n} \end{bmatrix}$$

$$\mathbf{J}_p = \begin{bmatrix} -a_1 s_1 - a_2 s_{12} & -a_2 s_{12} & 0 \\ a_1 c_1 + a_2 c_{12} & a_2 c_{12} & 0 \\ 0 & 0 & -1 \end{bmatrix}$$

Prismatic Joints



$$\dot{o}_n^0 = \dot{d}_i R_{i-1}^0 \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \dot{d}_i z_{i-1}^0$$

$$J_{v_i} = z_{i-1}$$

Figure 4.1: Motion of the end effector due to prismatic joint i .

Revolute Joints

$$v = \omega \times r$$

$$\omega = \dot{\theta}_i z_{i-1}$$

$$r = o_n - o_{i-1}$$

$$J_{v_i} = z_{i-1} \times (o_n - o_{i-1})$$

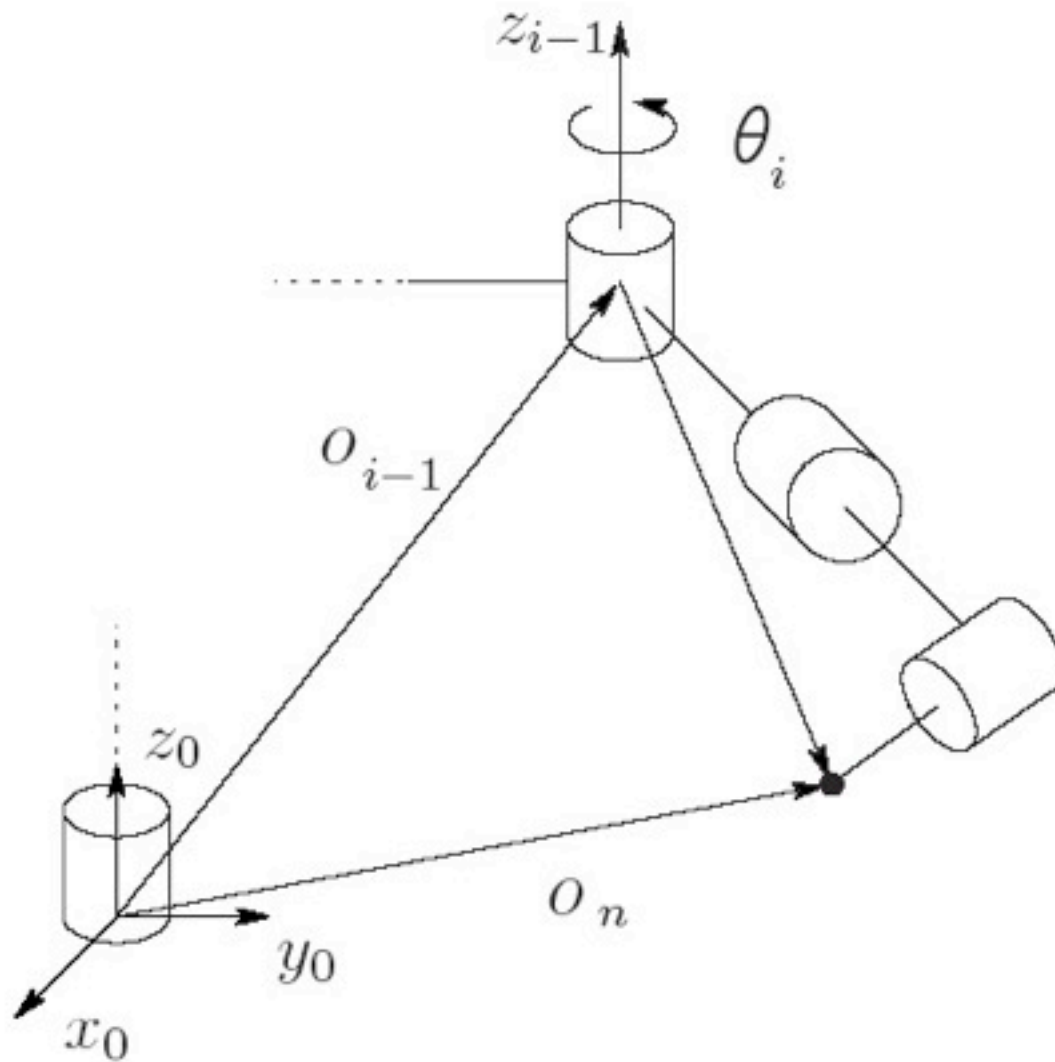


Figure 4.2: Motion of the end effector due to revolute joint i .

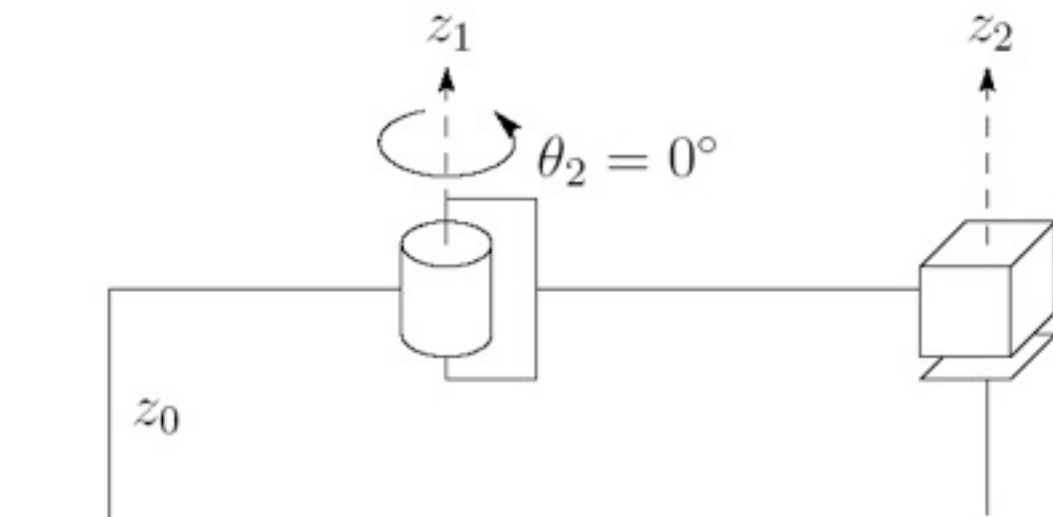
Prismatic Joints

$$J_{v_i} = z_{i-1}$$

Revolute Joints

$$J_{v_i} = z_{i-1} \times (o_n - o_{i-1})$$

Another way to construct the position Jacobian.



$$\mathbf{J}_p = \begin{bmatrix} -a_1 s_1 - a_2 s_{12} & -a_2 s_{12} & 0 \\ a_1 c_1 + a_2 c_{12} & a_2 c_{12} & 0 \\ 0 & 0 & -1 \end{bmatrix}$$

Questions ?

Singularities are points in the configuration space where infinitesimal motion in a certain direction is not possible and the manipulator loses one or more degrees of freedom

Mathematically, singularities exist at any point in the workspace where the Jacobian matrix loses rank.

a matrix is singular if and only if its determinant is zero:

$$\det(\mathbf{J}) = 0$$

when operating at a singular point, **bounded end-effector velocities** may correspond to **unbounded joint velocities**

singularities are often found on the edges of the workspace, and also relate to non-unique solutions to the inverse kinematics